

National Aeronautics and Space
Administration



Design of a Propeller with Global Minimum Torque

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Problem/Need

➤ Problem/Need

- **Advanced Air Mobility (AAM)**
 - Improved transportation method for public
- **Urban Air Mobility (UAM) vehicles**
 - Technological viability
 - Public acceptance

➤ Goal/Gap

- Improve Noise Pollution
- Improve Vehicle Efficiency



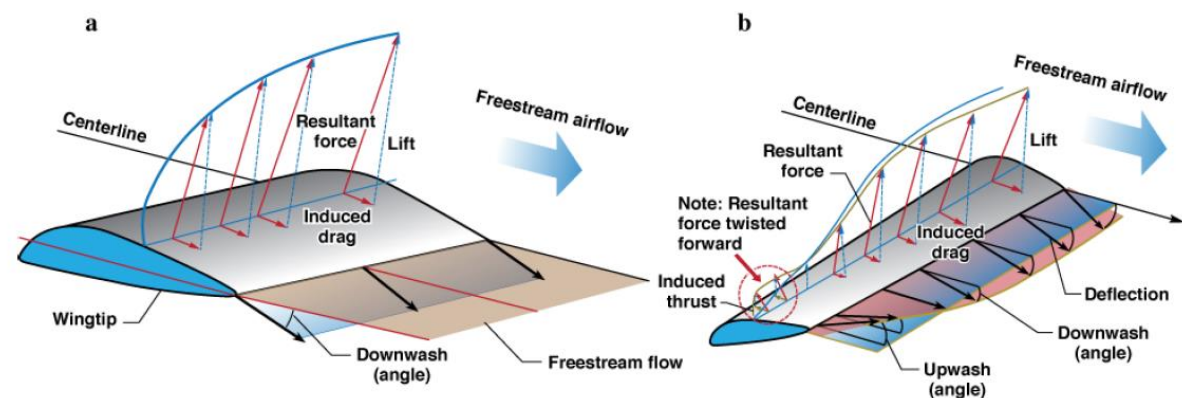
Fig. 1: AAM Futuristic City-scape [1]



Fig. 2: LA-8 VTOL Vehicle [2]

➤ Prandtl Wing “Bell” Span-load Theory

- Developed by Al Bowers
- Non-elliptical span-loading of wings
- References:
 - NASA/TP–2016219072
 - NASA/TM–20210014683
 - NASA Patent: 9,382,000
 - NASA Patent: 10,414,485



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Fig. 3: Comparison of forces between traditional elliptical span-load (a) and Bell “Prandtl” span-load (b) [3]

Background/Motivation

➤ Adapted to propeller design

- **Power In / Thrust Out**
 - Total Thrust Kept Constant → Minimize Total Torque
 - Calculus of Variations Optimization
- **Global 3D solution of minimum torque**
 - Max lift coefficient inboard along blade-span then taper at ~72% span to ~20% lift
 - Reduced blade tip loading → reduces large shear layer intensity [4] → reduces noise

➤ Trade Robustness for Efficiency

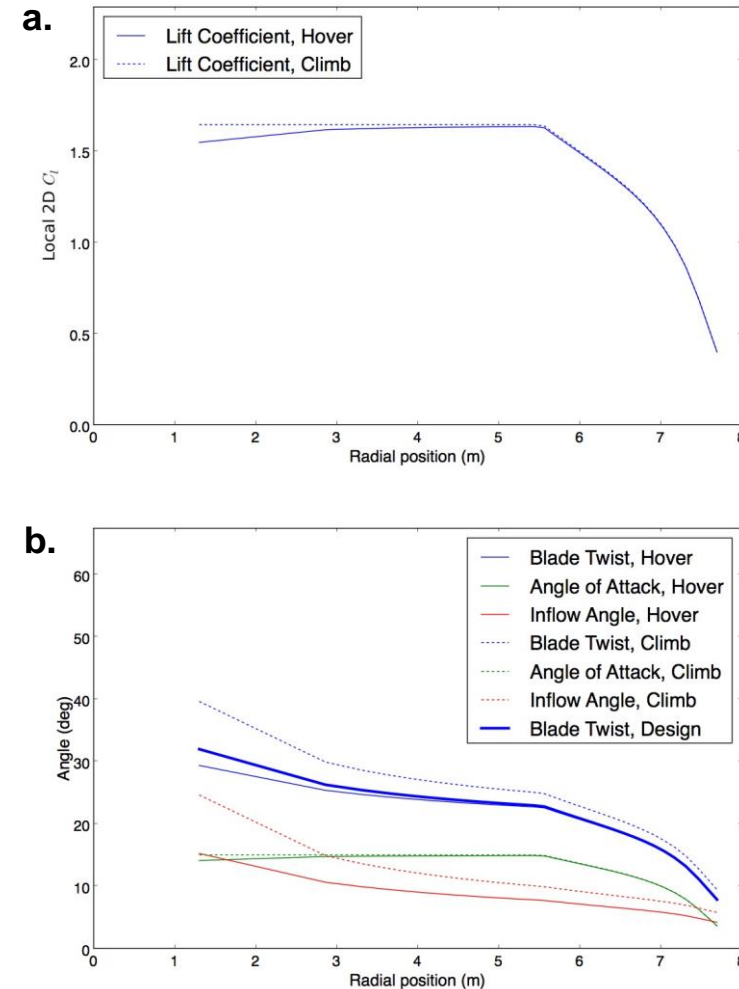


Fig. 4: Lift coefficient (a) and blade twist (b) characterization of 3D optimized propeller lift circulation



Design Methodology



- **Baseline Comparison Design:**
 - *Minimum Induced Loss (MIL)*

- **Constants (MIL vs Novel “Prandtl”):**
 - Diameter
 - “Pitch”
 - Advance Ratio Design Point
 - Chord Distribution
 - Camber Distribution of Airfoil
 - Material and Manufacturing
 - Drive System (Motors, ESCs, mounts, etc.)
 - Instrumentation

- **Differences (MIL vs Novel “Prandtl”):**
 - **Twist Distribution (C_L / AOA)**



Design Methodology



➤ Novel “Prandtl” Blade Design (Incremental Approach)

- **Phase I**
 - Bowers' C_L Optimization → Blade Twist
 - Constant Chord
 - Constant Airfoil Distributions
- **Phase II**
 - Bowers' C_L Optimization → Blade Twist
 - Constant Chord
 - Non-Constant Airfoil Distributions
- **Phase III**
 - Bowers' C_L Optimization → Blade Twist
 - Non-Constant Chord
 - Non-Constant Airfoil Distributions

➤ Airfoil Choice

- **Optimized for Inboard Section**
 - Near Max C_L Operating Condition
- **Two Standard Options**
 - NACA 6412
 - Slightly higher max C_L
 - MH 115
 - Good Stall Characteristics
 - Higher max C_L/C_D

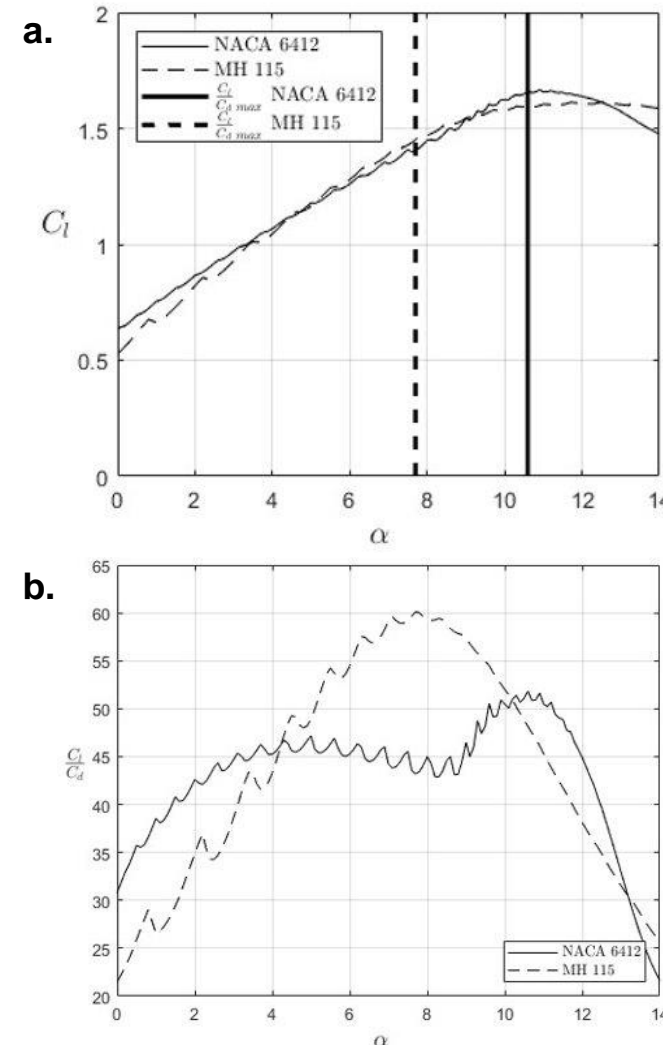


Fig. 5: C_L vs α (a) and C_L/C_D vs α (b) characterization of NACA 6412 vs MH 115 Airfoils

Phase I Design

➤ Parameters

- 2-Bladed
- **18-inch Diameter**
- **Advance Ratio Design Point**
 - *0.4*
- **RPM Design Point**
 - *3000*
- **Freestream Velocity Design Point**
 - *9.144 m/s*
- **Blade Twist Based on Bowers' C_L Optimization**
- **Constant Chord**
- **Constant Airfoil**

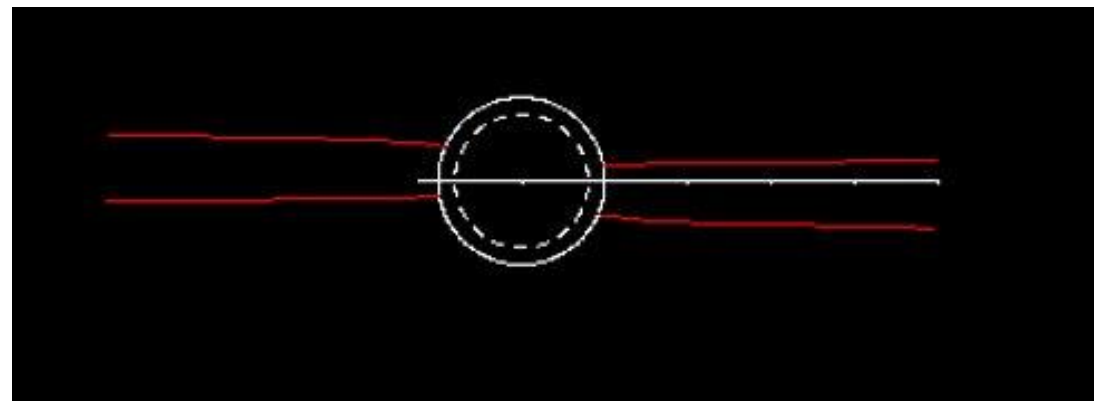


Fig. 6: XROTOR Representation of Phase I Propeller

Phase II Design

➤ Airfoil Choice

- Decreasing Camber for Tip Airfoil
- Non-linear Transition from Root Airfoil to Tip Airfoil
- Less Twist Necessary at Tip
 - Less Cambered Airfoil Reduced Tip Loading Instead of Angle of Attack (Twist)

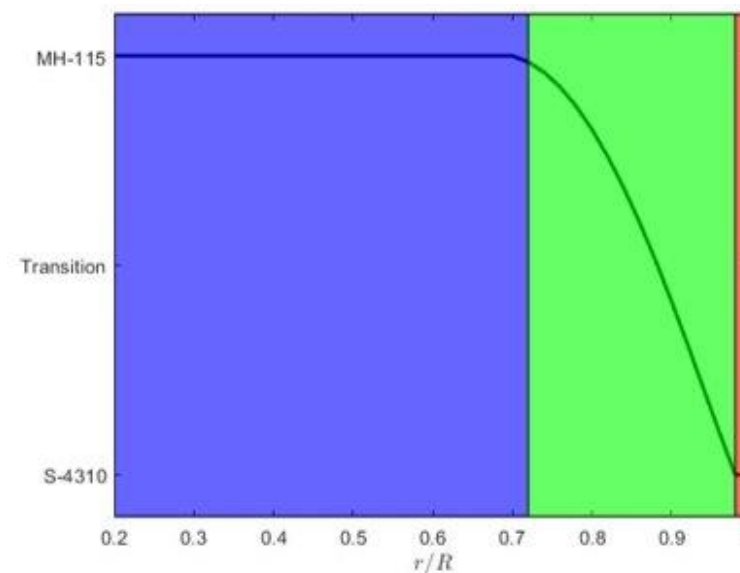
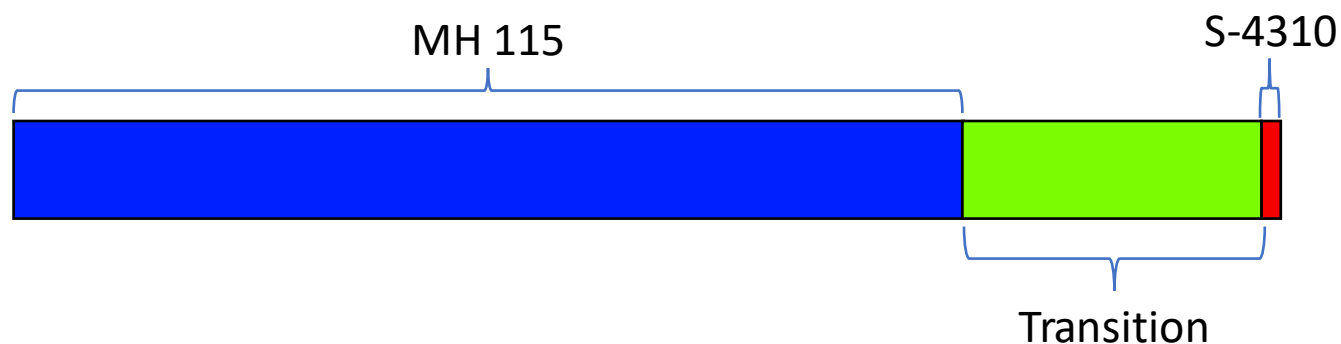


Fig. 7: Airfoil Distribution of Phase II Design: Inboard, Non-linear Transition, and Outboard Airfoils

➤ Parameters

- 18in (Same) Diameter
- Nonlinear Airfoil Distribution
- Exchanging Max C_L for Twist

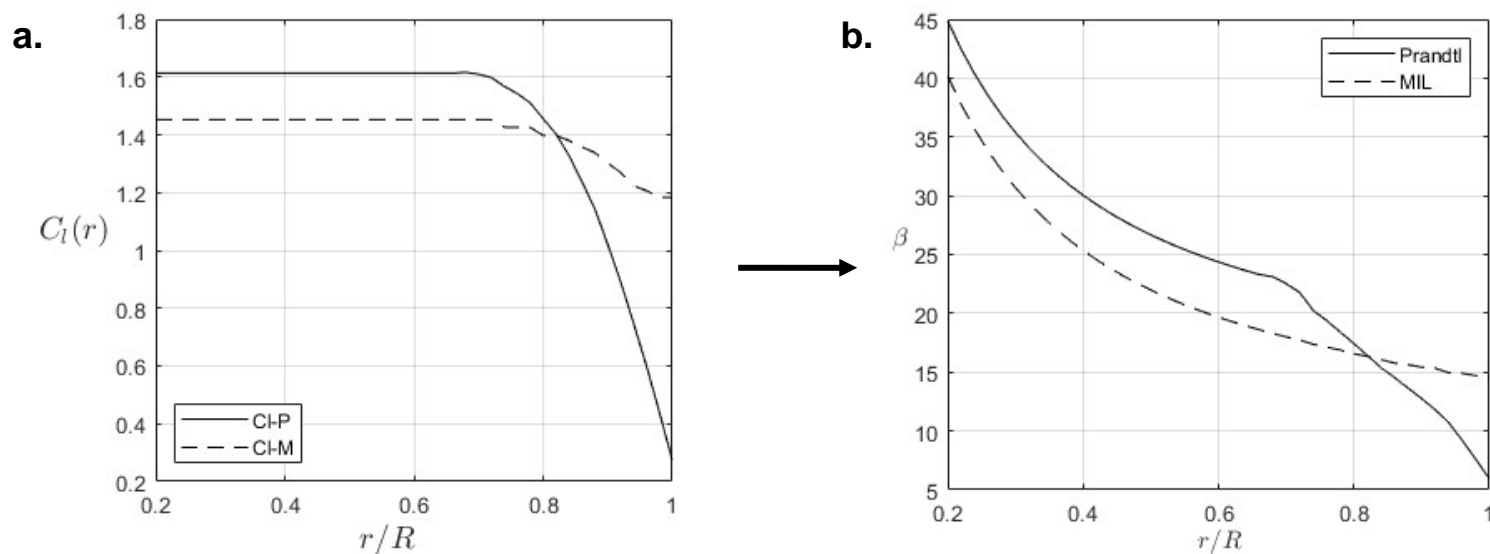


Fig. 8: C_L (a) and blade twist – β (b) of Phase II Design

Phase III (Final) Design

Parameters

- 18in (Same) Diameter
- Same Airfoil Distribution
- Chord Distribution Changes

Conclusions

- Efficiency Increase: ~2%

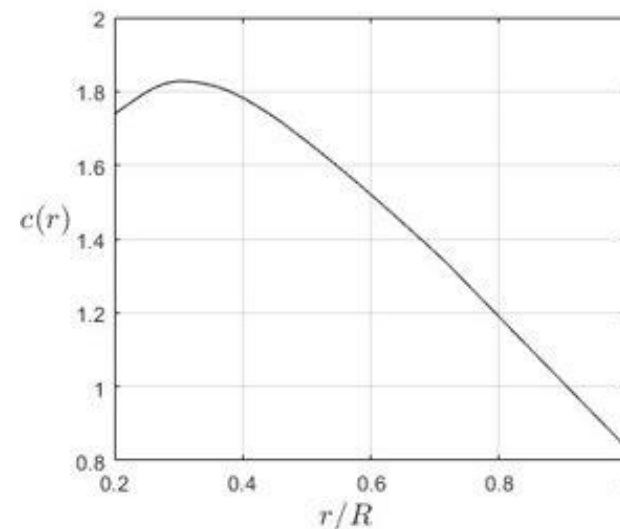


Fig. 9: Chord Distribution of Phase III Design

Table 1: 3000 RPM XROTOR Results for MIL (Baseline) and Prandtl (Novel) Propellers

	MIL	Prandtl
Thrust (N)	19.8	19.4
Torque (Nm)	1.02	0.98
C_T	0.14802	0.14468
C_P	0.10447	0.10056
Efficiency	0.5667	0.5754

Phase III (Final) Design Summary

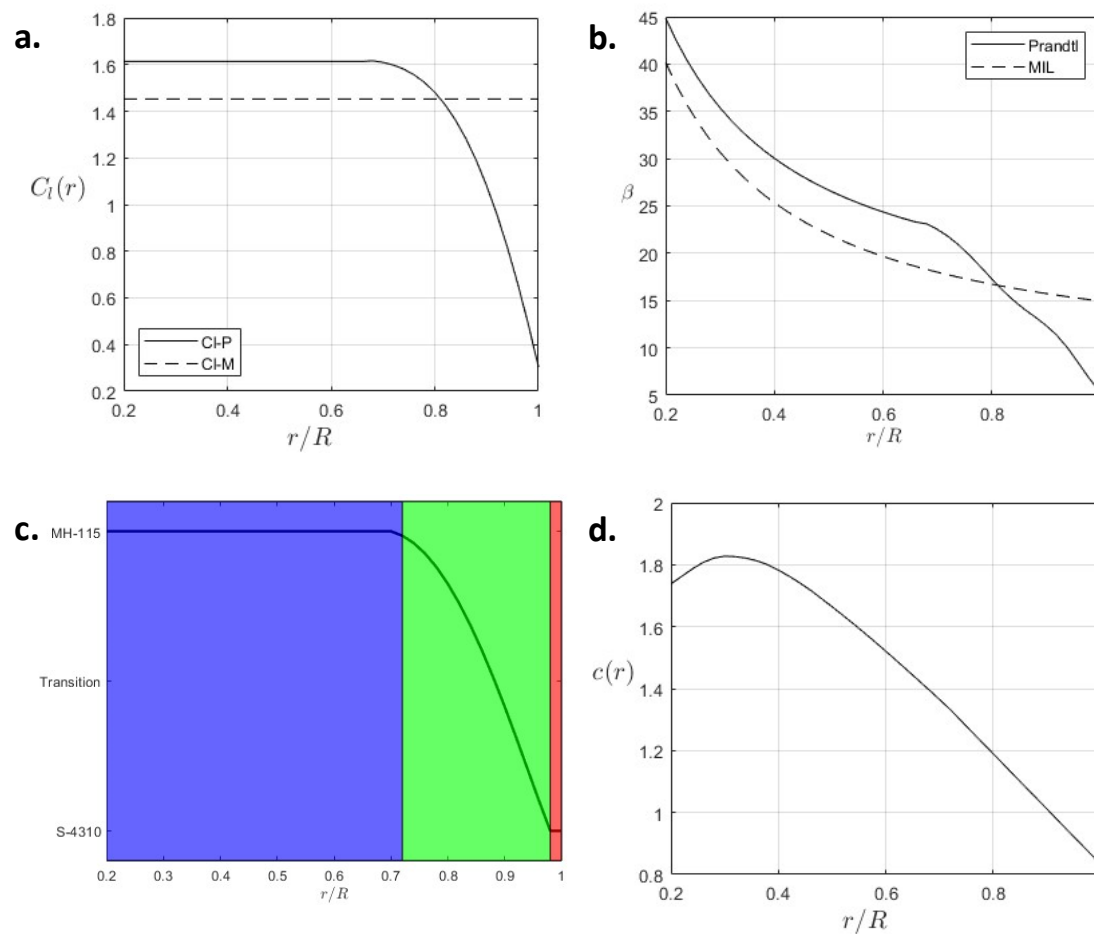


Fig. 10: Final (Phase III) Design of Prandtl and MIL propeller (a) Coefficient of Lift (C_l) distribution, (b) blade twist (β) distribution, (c) airfoil distribution, and (d) chord distribution

Combination Designs

➤ Back off “100%” solution

- Design in more robustness
- Percentage between MIL and Prandtl blade twist along blade span

➤ 7 Designs:

- 100% MIL (baseline)
- 100% Prandtl
- Combo 1: 50% Prandtl / 50% MIL (“5050”)
- Combo 2: 60% Prandtl / 40% MIL (“6040”)
- Combo 3: 70% Prandtl / 30% MIL (“7030”)
- Combo 4: 80% Prandtl / 20% MIL (“8020”)
- Combo 5: 90% Prandtl / 10% MIL (“9010”)

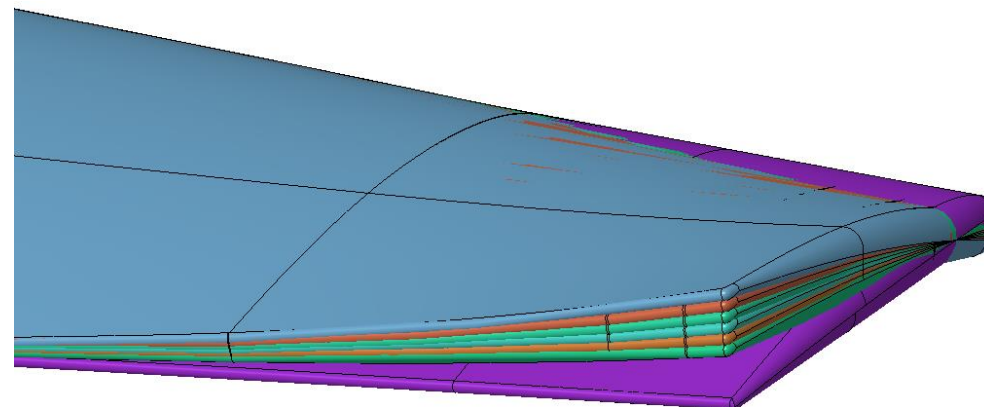


Fig. 11: Tip blade twists of MIL (purple) to Prandtl (blue) propeller blades with combo blades in-between.

Results (Final Design)

- **Advance Ratio Sweep – Prandtl, MIL, and Combo Blades**
 - **3000 RPM for All Runs**

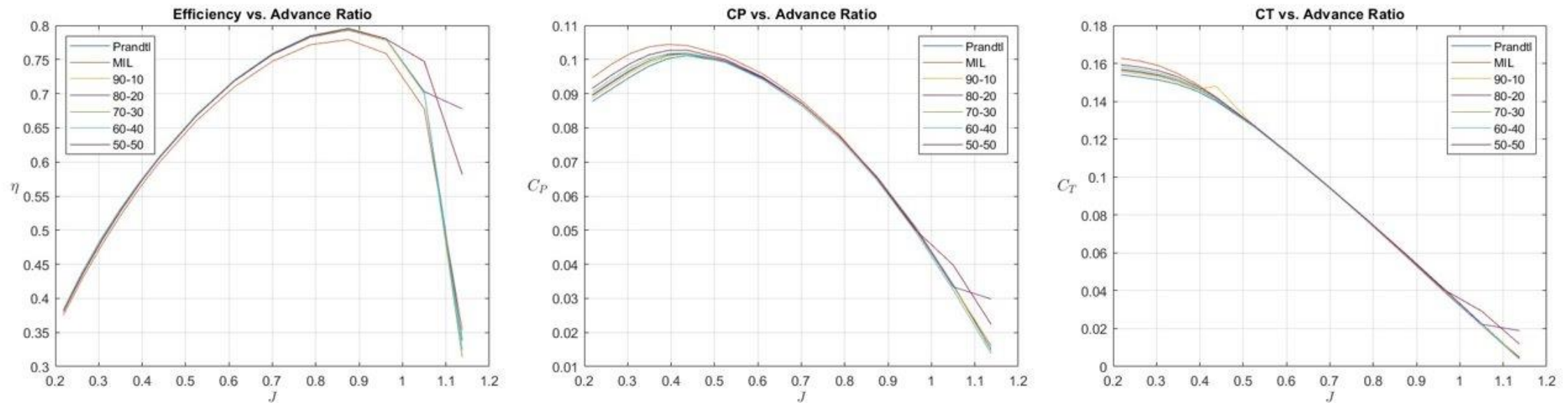


Fig. 12: Efficiency, C_P , and C_T vs Advance Ratio of MIL, Prandtl, and all Combo Propeller Designs

Results (Final Design)

➤ Advance Ratio Sweep – Prandtl Only

- 2000, 3000, 4000, 6000, 8000 RPM

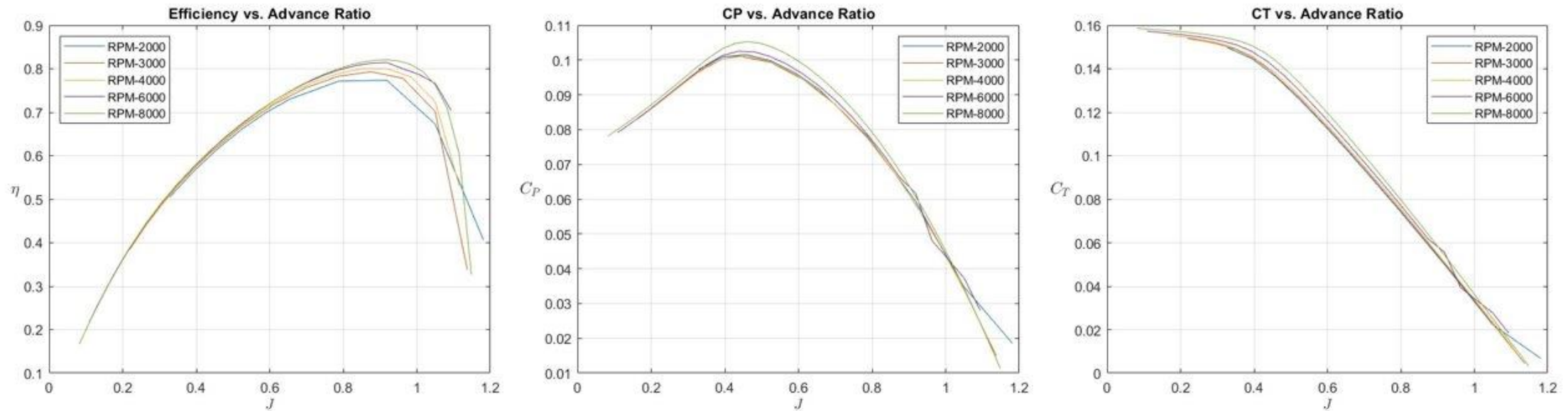


Fig. 13: Efficiency, C_P , and C_T vs Advance Ratio of Prandtl Design and Various RPMs



Future Work



- **Further Design Optimization**
 - Airfoil Choice for Full-Scale → Not as Concerned with Reynold's Number Properties
 - Optimize Chord Distribution for Efficiency/Acoustics
- **CFD Analysis of Propeller Blades to Determine Flow Field**
- **Acoustic Wind Tunnel Testing**
 - Low Speed Acoustic Wind Tunnel (LSAWT) at NASA Langley
- **Real-world Testing and Applicability of Propeller**
 - Robustness vs Efficiency Tradeoff



References



- [1] NASA RVLT Project (<https://www.nasa.gov/directorates/armd/aavp/rvlt/>)
- [2] North, David, D., Busan, Ronald, C., Howland, Greg, “Design and Fabrication of the Langley Aerodrome No. 8 Distributed Electric Propulsion VTOL Testbed”, NASA TM-20205011023, January 2021.
- [3] Bowers, Albion, H., Murillo, Oscar, J., et al., “On Wings of the Minimum Induced Drag: Spanload Implications for Aircraft and Birds”, NASA TP-2016219072, March 2016.
- [4] Marte, Jack E., and Donald W. Kurtz, *A Review of Aerodynamic Noise From Propellers, Rotors, and Lift Fans*, NASA-CR-107568, January 1970.